

FORMULA SHEET (Module 1)

Motor model (Inputs: V_m, T_d ; Outputs: ω_m, I_m): $V_m = R_m I_m + L_m \frac{dI_m}{dt} + V_{emf}$; $V_{emf} = k_m \omega_m (1 + \tau_m \omega_m)$
 $J_{eq} \frac{d\omega_m}{dt} = T_m - T_d$; $T_m = k_t (I_m - I_f) = k_t [I_m - I_0 \text{sgn}(\omega_m) - I_1 \omega_m - I_2 \omega_m^2]$; **Simplified:** $\omega_m = \frac{1}{J_{eq} s + \frac{k_m^2}{R_m}} \left(\frac{k_m}{R_m} V_m + T_d \right)$

LSE: $Y_N = A_N \theta \Rightarrow \hat{\theta}_N = (A_N^T A_N)^{-1} A_N^T Y_N$

$$\sum_{j=0}^n a_j y(k-j) = \sum_{j=0}^n b_j u(k-j), \text{ and WLOG } a_0 = 1 \Rightarrow y(k) = \frac{[-y(k-1) \dots -y(k-n) \ u(k) \dots u(k-n)]}{h^T(k)} \begin{bmatrix} a_1 \\ \vdots \\ a_n \\ \vdots \\ b_n \end{bmatrix} \theta$$

Collect $n \leq k \leq N \Rightarrow$

$$\underbrace{\begin{bmatrix} y(n) \\ \vdots \\ y(k) \\ \vdots \\ y(N) \end{bmatrix}}_{Y_N}_{N-n+1 \times 1} = \underbrace{\begin{bmatrix} -y(n-1) \dots -y(0) \ u(n) \dots u(0) \\ \vdots \\ -y(k-1) \dots -y(k-n) \ u(k) \dots u(k-n) \\ \vdots \\ -y(N-1) \dots -y(N-n) \ u(N) \dots u(N-n) \end{bmatrix}}_{H_N}_{N-n+1 \times 2n+1} \underbrace{\begin{bmatrix} a_1 \\ \vdots \\ a_n \\ \vdots \\ b_n \end{bmatrix}}_{\theta}_{2n+1 \times 1}$$

$\Rightarrow \hat{\theta} = (H_N^T H_N)^{-1} H_N^T Y_N$

LTI: $y(t) = \int_{-\infty}^{\infty} h(t-\tau)u(\tau)d\tau \equiv h(t) * u(t) \leftrightarrow H(s)U(s) = U(s)H(s) \leftrightarrow u(t) * h(t) \equiv \int_{-\infty}^{\infty} u(t-\tau)h(\tau)d\tau$

ZOH discretization: $G(z) = Z[H_{zoh}(s)G(s)] = Z\left[\frac{1-e^{-sT}}{s}G(s)\right] = (1-z^{-1})Z\left[\frac{G(s)}{s}\right]$

Bilinear discretization: $s \approx \frac{2z-1}{Tz+1} \Leftrightarrow z \approx \frac{1+\frac{T}{2}s}{1-\frac{T}{2}s}$

Poles, $p = \sigma \pm j\omega$ \Rightarrow Time const, $\tau = \frac{1}{|\sigma|}$; Osc. freq, $\omega = \text{Im}(p)$; Nat. freq, $\omega_n = \sqrt{\sigma^2 + \omega^2}$; Damping ratio, $\zeta = -\sigma/\omega_n$

Note for a quadratic char. polynomial with poles at p_1, p_2 : $\omega_n^2 = p_1 p_2$; $\zeta = \frac{-(p_1+p_2)}{2\sqrt{p_1 p_2}}$

2nd-order TF, $\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \Rightarrow$ Poles: $\begin{cases} -\omega_n(\zeta \pm \sqrt{1-\zeta^2}); & (\zeta < 1) \\ -\omega_n; & (\zeta = 1) \\ -\omega_n(\zeta \pm \sqrt{\zeta^2-1}); & (\zeta > 1) \end{cases}$

Simple real poles, ie, over-damped $\Leftrightarrow \zeta > 1$: $1 - \left(\frac{\sqrt{\zeta^2-1}+\zeta}{2\sqrt{\zeta^2-1}}\right)e^{(-\zeta+\sqrt{\zeta^2-1})\omega_n t} - \left(\frac{\sqrt{\zeta^2-1}-\zeta}{2\sqrt{\zeta^2-1}}\right)e^{(-\zeta-\sqrt{\zeta^2-1})\omega_n t}$

Repeated real poles, ie, critically-damped $\Leftrightarrow \zeta=1$: $1 - e^{-\omega_n t}(1 + \omega_n t)$

Complex pair of poles, ie, under-damped $\Leftrightarrow \zeta < 1$: $1 - \left[\frac{1}{\sqrt{1-\zeta^2}}\right]e^{\sigma t}[\sin(\omega t + \cos^{-1} \zeta)]$; ($\sigma = -\zeta\omega_n$; $\omega = \sqrt{1-\zeta^2}\omega_n$)

Peak overshoot $e^{-\pi\zeta/\sqrt{1-\zeta^2}}$ @ half time-period, $\frac{\pi}{\omega} = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}}$; **Rise time** (time to reach 1): $\frac{\pi - \cos^{-1} \zeta}{\omega}$

Settling time (3-5 time-const): $\frac{3}{\omega_n\zeta}$ (5%); $\frac{4}{\omega_n\zeta}$ (2%); $\frac{5}{\omega_n\zeta}$ (1%); **BW:** $\omega_n\sqrt{[(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}]}$

Bode peak (@ $\omega_n\sqrt{1-2\zeta^2}$) = $\frac{1}{2\zeta\sqrt{1-\zeta^2}}$ (@ $\omega_n = \frac{1}{2\zeta}$); **Phase** (@ $\omega_n\sqrt{1-2\zeta^2}$) = $-\tan^{-1}\left(\frac{\sqrt{1-2\zeta^2}}{\zeta}\right)$ (@ $\omega_n = -90^\circ$)

Phase-margin, $|\angle L(j\omega_g)| - \pi = \tan^{-1}\left(\frac{2\zeta}{\sqrt{4\zeta^4+1-2\zeta^2}}\right)$; **Gain-margin,** $|20\log_{10}(L(j\omega_p))| = \infty$

	s-domain $e_{ss} = \lim_{s \rightarrow 0} s \left[\frac{R(s)}{1+L(s)} \right]$	z-domain $e_{ss} = \lim_{z \rightarrow 1} (z-1) \left[\frac{R(z)}{1+L(z)} \right]$
$N = 0$ (step-input) $\Rightarrow R(s) = \frac{1}{s}$ or $R(z) = \frac{z}{z-1}$	$\frac{1}{1 + \lim_{s \rightarrow 0} L(s)} \equiv \frac{1}{1 + K_0^s}$	$\frac{1}{1 + \lim_{z \rightarrow 1} L(z)} \equiv \frac{1}{1 + K_0^z}$
$N > 0 \Rightarrow R(s) = O\left(\frac{1}{s^{N+1}}\right)$ or $R(z) = O\left(\frac{T^N}{(z-1)^{N+1}}\right)$	$\frac{1}{\lim_{s \rightarrow 0} s^N L(s)} \equiv \frac{1}{K_N^s}$	$\frac{T^N}{\lim_{z \rightarrow 1} (z-1)^N L(z)} \equiv \frac{1}{K_N^z}$

Type = $N \Rightarrow e_{ss} = 1/(1 + K_N)$ and $1/K_N$ resp., for $O(t^0)$ and $O(t^N)$ inputs;

Type $> N \Rightarrow e_{ss} = 0 \wedge$ Type $< N \Rightarrow e_{ss} = \infty$ for $O(t^N)$ inputs;

Char. eq: $\chi(s) := \text{num}(1 + L(s)) = \text{num}(L(s)) + \text{den}(L(s))$

ZN Tuning of PID: $K_p = 0.6K_u, K_I = 1.2\frac{K_u}{T_u}, K_D = .075K_u T_u$

BIBO Stable $\Leftrightarrow \int_{-\infty}^{\infty} |h(t)|dt < \infty \Leftrightarrow$ All poles in LHP or if on imaginary-axis then non-repeating

Internally Stable \Leftrightarrow All eigenvalues in LHP (asyp. stable) or if on imaginary-axis then grade-1

FORMULA SHEET (Module 2)

Lagrangian: $L = KE - PE; \frac{\partial^2 L}{\partial t \partial q_i} - \frac{\partial L}{\partial q_i} = F_i$ OR τ_i (when q_i is linear OR angular position)

Linearization: $\dot{x}(t) = f(x(t), u(t), t); y(t) = h(x(t), u(t), t)$ is at equilibrium at x^* if $\exists u^*(t): f(x^*, u^*(t), t) = 0$. The linearized system matrices at the equilibrium are given by:

$$A(t) \equiv \left. \frac{\partial f}{\partial x} \right|_{x^*, u^*(t)} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \dots & \frac{\partial f_1}{\partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1} & \dots & \frac{\partial f_n}{\partial x_n} \end{bmatrix}, B(t) \equiv \left. \frac{\partial f}{\partial u} \right|_{x^*, u^*(t)} = \begin{bmatrix} \frac{\partial f_1}{\partial u_1} & \dots & \frac{\partial f_1}{\partial u_m} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial u_1} & \dots & \frac{\partial f_n}{\partial u_m} \end{bmatrix},$$

$$C(t) \equiv \left. \frac{\partial h}{\partial x} \right|_{x^*, u^*(t)} = \begin{bmatrix} \frac{\partial h_1}{\partial x_1} & \dots & \frac{\partial h_1}{\partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial h_p}{\partial x_1} & \dots & \frac{\partial h_p}{\partial x_n} \end{bmatrix}, D(t) \equiv \left. \frac{\partial h}{\partial u} \right|_{x^*, u^*(t)} = \begin{bmatrix} \frac{\partial h_1}{\partial u_1} & \dots & \frac{\partial h_1}{\partial u_m} \\ \vdots & \ddots & \vdots \\ \frac{\partial h_p}{\partial u_1} & \dots & \frac{\partial h_p}{\partial u_m} \end{bmatrix}.$$

Transfer function: $G(s) \equiv G_{sp}(s) + G(\infty)$, with $G_{sp}(s) = C(sI - A)^{-1}B$ and $G(\infty) = D$.

State-space: $G(s) = \frac{Y(s)}{U(s)} = \frac{b_n s^n + \dots + b_0}{a_n s^n + \dots + a_0} = \frac{b'_{n-1} s^{n-1} + \dots + b'_0}{s^n + a'_{n-1} s^{n-1} + \dots + a'_0} + \frac{b_n}{a_n}$, its **companion form** state-space realization is:

$$A = \begin{bmatrix} 0 & 1 & \dots & \dots & 0 \\ 0 & 0 & 1 & \dots & \vdots \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a'_0 & -a'_1 & \dots & \dots & -a'_{n-1} \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 1 \end{bmatrix}, C = [b'_0 \ b'_1 \ \dots \ b'_{n-1}], D = \begin{bmatrix} b_n \\ a_n \end{bmatrix}.$$

State-eq solution: $x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau) d\tau$, where $e^{At} \leftrightarrow (sI - A)^{-1}$

State change: $z(t) = Px(t) \Rightarrow \hat{A} = P^{-1}AP; \hat{B} = P^{-1}B; \hat{C} = CP; \hat{D} = D$.

Control input for steering initial state to final state: $u(t) = -B^T e^{A^T(t_f - t)} W_c^{-1}(t_f) [e^{At_f}x(0) - x(t_f)]$, where $t_f > 0$ is the final time, and $W_c(t_f) = \int_0^{t_f} e^{A\tau} B B^T e^{A^T \tau} d\tau$.

Controllability matrix: $T = [B \ AB \ A^2B \ \dots \ A^{n-1}B]$.

Map to companion form: Use similarity transform, $P = T\bar{T}^{-1}$ (works for controllable system).

State-feedback using companion form: Given $\chi_A(s) = s^n + a_{n-1}s^{n-1} + \dots + a_0$, and desired $\chi_d(s) = s^n + \tilde{a}_{n-1}s^{n-1} + \dots + \tilde{a}_0$. Then, $\bar{K} = [(\tilde{a}_0 - a_0) \ (\tilde{a}_1 - a_1) \ \dots \ (\tilde{a}_{n-1} - a_{n-1})]$ and $K = \bar{K}P^{-1} = \bar{K}\bar{T}\bar{T}^{-1}$ are such that

$$\chi_{\bar{A} - \bar{B}\bar{K}}(s) = \chi_d(s) = \chi_{A - BK}(s).$$

Ackermann's formula for state feedback control: $K = [0 \ 0 \ \dots \ 1]T^{-1}\chi_d(A)$.

Observability matrix: $O = \begin{bmatrix} C \\ \vdots \\ CA^{n-1} \end{bmatrix}$.

State Estimator/Observer: $[\hat{x} = A\hat{x} + Bu + L(y - \hat{y}) \wedge \dot{\hat{y}} = C\hat{x} + Du] \Rightarrow \dot{e} = (A - LC)e$, where $e = x - \hat{x}$.

Synthesis of L^T is like the synthesis of K with (A, B) replaced by (A^T, C^T) . Once L^T is found, take the transpose to get L .

Lyapunov function: It's a positive function with negative rate: $V(x - x^*) \geq 0 \wedge \dot{V}(x - x^*) < 0 \wedge V(0) = \dot{V}(0) = 0$, where x^* is equilibrium.

For linear system, $\dot{x} = Ax$, it's equilibrium is $x^* = 0$, and one can choose $V(x - x^*) = V(x) = x^T Px$. Then $\dot{V}(x) = \dot{x}^T Px + x^T P\dot{x} = x^T A^T Px + x^T PAx < 0$ iff $A^T P + PA < 0$ iff $\exists Q > 0: A^T P + PA = -Q$ and $V(x) = x^T Px \geq 0$ iff $P \geq 0$ (NOTE: $P \geq 0$ if all its eigenvalues are non-negative, and $Q > 0$ if all its eigenvalues are positive.)

Sliding mode control: For a sliding surface $s = 0$, consider energy function $V = \frac{1}{2} s^T s$

$$\Rightarrow \dot{V} = s^T \dot{s} = s^T \frac{\partial s}{\partial x} \dot{x} = s^T \frac{\partial s}{\partial x} f(x, u). \text{ Choose } u \text{ so that } \text{sgn}(f(x, u)) = -\text{sgn}\left(s^T \frac{\partial s}{\partial x}\right) \Rightarrow \dot{V} \leq 0.$$

FORMULA SHEET (Module 3)

Rotation Matrix is Unitary, ie, $R^{-1} = R^T \wedge \det(R) = 1$

2D rotation; rotation+translation: $R_z(\psi) = \begin{bmatrix} \cos \psi & -\sin \psi \\ \sin \psi & \cos \psi \end{bmatrix}; T(\psi; \begin{bmatrix} x_t \\ z_t \end{bmatrix}) = \begin{bmatrix} \cos \psi & -\sin \psi & x_t \\ \sin \psi & \cos \psi & y_t \\ 0 & 0 & 1 \end{bmatrix}$

3D rotation: $R(\phi, \theta, \psi) = R_z(\psi)R_y(\theta)R_x(\phi) = \begin{bmatrix} \cos \theta \cos \psi & \sin \phi \sin \theta \cos \psi - \cos \phi \sin \psi & \cos \phi \sin \theta \cos \psi + \sin \phi \sin \psi \\ \cos \theta \sin \psi & \sin \phi \sin \theta \sin \psi + \cos \phi \cos \psi & \cos \phi \sin \theta \sin \psi - \sin \phi \cos \psi \\ -\sin \theta & \sin \phi \cos \theta & \cos \phi \cos \theta \end{bmatrix}$

Quadcopter model:
$$\left. \begin{aligned} m\ddot{x} &= (\cos \phi \sin \theta \cos \psi + \sin \phi \sin \psi)u_1 \\ m\ddot{y} &= (\cos \phi \sin \theta \sin \psi - \sin \phi \cos \psi)u_1 \\ m\ddot{z} &= (\cos \phi \cos \theta)u_1 - mg \\ I_{xx}\ddot{\phi} - (I_{yy} - I_{zz})\dot{\theta}\dot{\psi} + I_r\dot{\theta}\omega &= \ell u_2 \\ I_{yy}\ddot{\theta} - (I_{zz} - I_{xx})\dot{\psi}\dot{\phi} - I_r\dot{\phi}\omega &= \ell u_3 \\ I_{zz}\ddot{\psi} - (I_{xx} - I_{yy})\dot{\phi}\dot{\theta} &= \ell u_4 \end{aligned} \right\}, \text{ where: } \begin{cases} u_1 = K_T(\omega_1^2 + \omega_2^2 + \omega_3^2 + \omega_4^2) \\ u_2 = K_T(\omega_2^2 - \omega_4^2) \\ u_3 = K_T(\omega_1^2 - \omega_3^2) \\ u_4 = K_D(\omega_2^2 + \omega_4^2 - \omega_1^2 - \omega_3^2) \\ \omega = \omega_2 + \omega_4 - \omega_1 - \omega_3 \end{cases}$$

Quaternion, $q = a + ib + jc + kd$, with $i^2 = j^2 = k^2 = ijk = -1 \Rightarrow (ij = k, jk = i, ki = j) \wedge (ji = -k, kj = -i, ik = -j)$

Rotate p around u by δ : $p' = rpr^*$, with $r = \cos \frac{\delta}{2} + (u_x \sin \frac{\delta}{2})i + (u_y \sin \frac{\delta}{2})j + (u_z \sin \frac{\delta}{2})k$, where $u_x^2 + u_y^2 + u_z^2 = 1$.

Same rotation using $R_u(\delta) = \begin{bmatrix} \cos \delta + u_x^2(1 - \cos \delta) & u_x u_y(1 - \cos \delta) - u_z \sin \delta & u_z u_x(1 - \cos \delta) + u_y \sin \delta \\ u_x u_y(1 - \cos \delta) + u_z \sin \delta & \cos \delta + u_y^2(1 - \cos \delta) & u_y u_z(1 - \cos \delta) - u_x \sin \delta \\ u_z u_x(1 - \cos \delta) - u_y \sin \delta & u_y u_z(1 - \cos \delta) + u_x \sin \delta & \cos \delta + u_z^2(1 - \cos \delta) \end{bmatrix}$

Attitude & altitude PID:
$$\left. \begin{aligned} u_1 &:= K_{P_z} \bar{z} + K_{I_z} \int \bar{z} + K_{D_z} \frac{d\bar{z}}{dt} \\ u_2 &:= K_{P_\phi} \bar{\phi} + K_{I_\phi} \int \bar{\phi} + K_{D_\phi} \frac{d\bar{\phi}}{dt} \\ u_3 &:= K_{P_\theta} \bar{\theta} + K_{I_\theta} \int \bar{\theta} + K_{D_\theta} \frac{d\bar{\theta}}{dt} \\ u_4 &:= K_{P_\psi} \bar{\psi} + K_{I_\psi} \int \bar{\psi} + K_{D_\psi} \frac{d\bar{\psi}}{dt} \end{aligned} \right\} \text{where } \bar{z} := z - z_a; \bar{\phi} := \phi - \phi_a; \bar{\theta} := \theta - \theta_a; \bar{\psi} := \psi - \psi_a$$

Position & yaw PID = Same as above PID with: $\phi_a = \tan^{-1} \left(\frac{\bar{x} \sin \psi - \bar{y} \cos \psi}{\sqrt{(\bar{x} \cos \psi + \bar{y} \sin \psi)^2 + \bar{z}^2}} \right) \wedge \theta_a = \tan^{-1} \left(\frac{\bar{x} \cos \psi + \bar{y} \sin \psi}{\bar{z}} \right)$

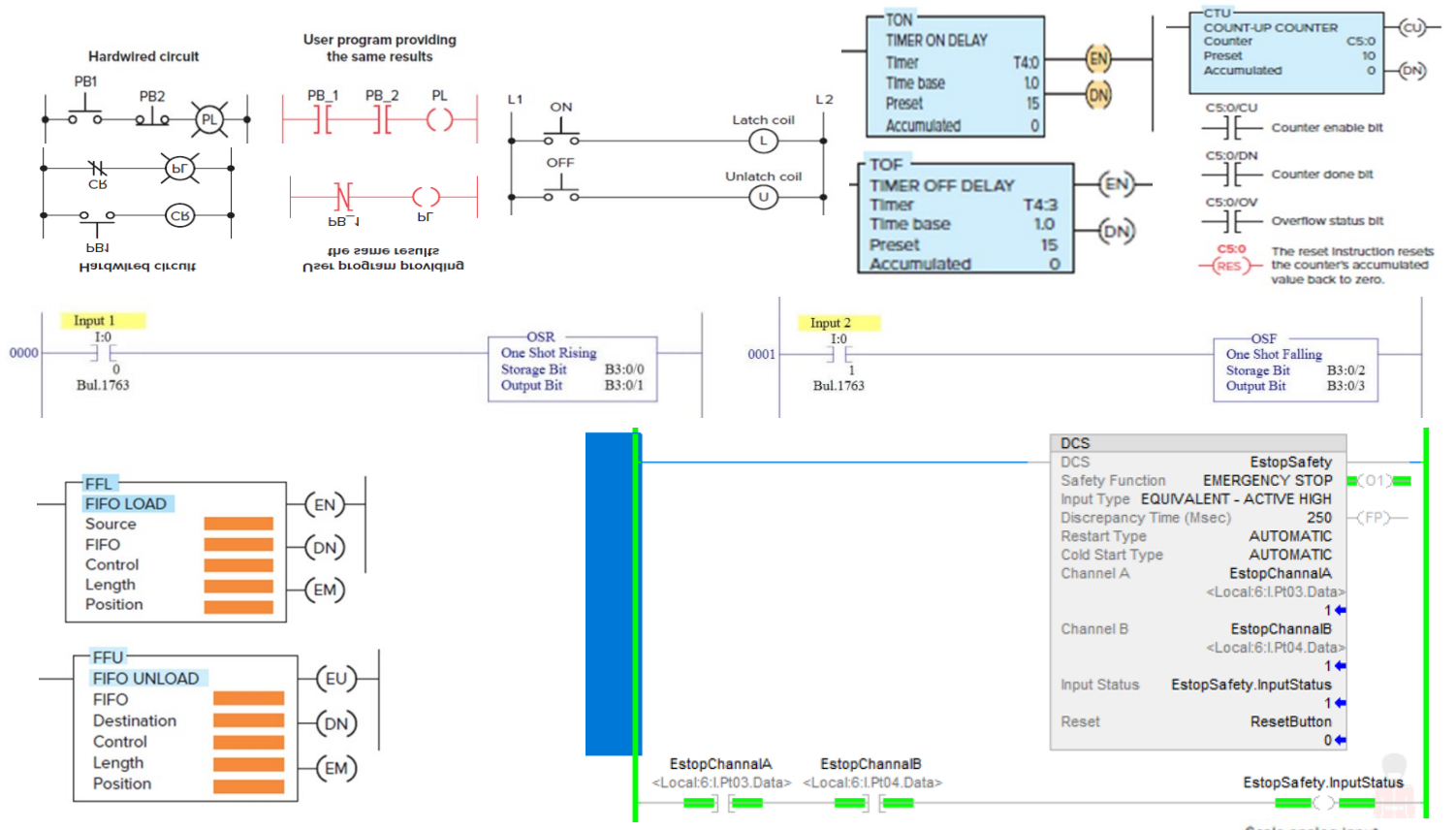
Kalman Filter:

$$\left. \begin{aligned} R_e(k+1) &= AR_e(k)A^T + R_\omega(k) \\ G(k+1) &= R_e(k+1)C^T [CR_e(k+1)C^T + R_v(k+1)]^{-1} \\ R_e(k+1) &= (I - G(k+1)C)R_e(k+1) \end{aligned} \right\} \wedge \begin{cases} \bar{x}(k+1) = A\hat{x}(k) + Bu(k) \\ \bar{y}(k+1) = C\bar{x}(k+1) + Du(k+1) \\ \hat{x}(k+1) = \bar{x}(k+1) + G(k+1)[y(k+1) - \bar{y}(k+1)] \end{cases}$$

FORMULA SHEET (Module 4)

Inputs: XIC, XIO

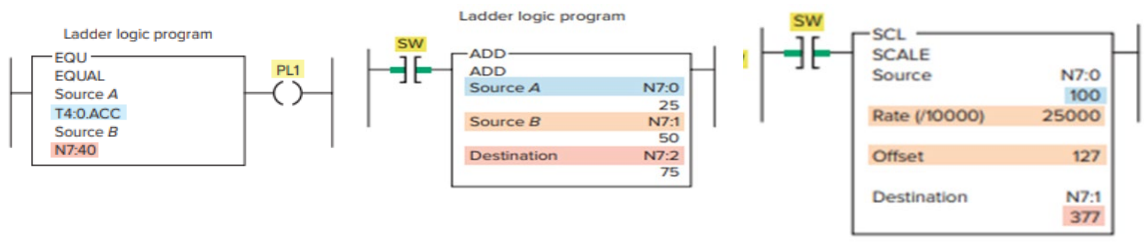
Outputs: OTE, Latch/Unlatch, Timer: On-delay vs Off Delay, Counter, One-shot Rising vs Falling, FIFO, DCS



Inputs: Compare with Source A and Source B (EQU, NEQ, GRT, GEQ, LES, LEQ)

Outputs: Ops with Sources/inputs & Destination/Output (MOV, ADD, SUB, MUL, DIV, MOD, SQR, SCL, SCP)

Program Controls: Output/Input pairs (JMP/LBL, JSR/RET)



SCALE W/PARAMETERS	
Input	I:1.0
Input Min.	0 <
Input Max.	32767 <
Scaled Min.	0
Scaled Max.	1000 <
Scaled Output	N7:20
	0 <